Modeling and Simulating Vortex Pinning and Transport Currents for High Temperature Superconductors

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Outline

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Superconductivity and Motivation

What is Superconductivity?



 Normal Metal Vs. Superconductor: Temperature

How does this Occur

• Below *T_c* the electrons form pairs (top).

• Movement is orderly.

No waste heat!

• Above T_c things break down (bottom).



Modeling SC

The Meissner Effect

- Occurs when a superconductor (SC) is in a magnetic field.
- A resistance free current (super current) is induced.
- The current prevents penetration.
- This persists until the field reaches a critical strength H_c .
- Magnetic Field Penetration = NO Superconductivity.



Type I and Type II

- Type I SC are not penetrated at all (Meissner Effect) (top right).
- Type II SC are only penetrated by tubes of magnetic flux (Vortices) (bottom).
- Two critical *H* values, *H*_{c1} and *H*_{c2}.



• Vortex state: $H_{c1} < H < H_{c2}$. Figure : Normal and Type I (top). Type II (bottom)

Why You Should Care: Applications

Possible Superconducting Technology:

- Efficient Current Carriers
- Powerful Magnets (by magnetization)

• Efficient Mag Lev

MRI



- There is no free lunch.
- T_c is close to 0 K for most metals.
- Liquid helium is expensive.
- This rules out many applications such as power wires.
- Thankfully recent discoveries have overcome this.

High Temperature Superconductors (HTS)

- New materials have revitalized superconductivity.
- Higher *T_c* values allow the use of liquid N or O coolants.
- Magnesium Diboride (MgB₂) is cheap and ductile (*T_c* = 39 K or -234° C).
- HgBa₂Ca₂Cu₃O₈ is used in MRIs ($T_c = 135$ K or -138° C).
- Hydrogen Sulfide under 150 G. Pascals of pressure ($T_c = 203$ K or -70° C).



High Temperature Superconductors (HTS)

- These materials come with new odd properties:
- Odd temperature dependencies in quantities.
- All of are Type II S.C.
- This complicates the modeling process.



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Modeling SC

Visualizing Vortices



Figure : SEM image of vortices

Figure : Simulation

- So far we have T_c and H_c .
- What happens when we apply a current to a SC?
- Can it be carried without Resistance?
- Only below J_c !

Why Vortex Dynamics are Important

- Vortices (B) and Current (J)= Flux Flow.
- Moving Vortices (flux flow) creates Resistance.

 $f \ \hat{\mathbf{x}} = J \ \hat{\mathbf{y}} \times B \ \hat{\mathbf{z}}$ $E \ \hat{\mathbf{y}} = B \ \hat{\mathbf{z}} \times u \ \hat{\mathbf{x}}$

- Flux Flow induces Electric Field (E) and Voltage (V).
- Resistance now exists $(\frac{V}{I} = R)$.



Vortex Pinning Comes to the Rescue

- Immobilizing the Vortices Is Crucial.
- Non Superconducting Metal=
 Normal Metal= Pinning Sites. (Outlined in Black)
- Vortices "Stick" To impurities.
- Limited increase In J_c.



Simulations

- Simulations are critical to modeling new technology.
- No models for two-band SC and vortex pinning by impurities.
- Larger domains to avoid boundary effects.



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- A model: the Ginzburg-Landau model.
- Modify it for HTS and vortex pinning.
- Specify a material and model it.
- Modify for large scale simulations.



Ginzburg-Landau

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Ginzburg-Landau (GL) Theory

- The G-L theory (or model) describes superconductivity as a phase transition for a valid temperature range.
- A free energy functional is formed.
- Its minimum is given by the G-L equations.
- This is done using calculus of variations.
- Gauge invariance.
- The model is non-dimensionalized using important material parameters.

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- Two variables:
 - ψ -The complex order parameter, describes the density of superconducting electrons.
 - A The magnetic vector potential, ∇ × A = B.
- Three material parameters:
 - λ -The penetration depth.
 - ξ The coherence length.
 - κ The G-L parameter $\kappa = \frac{\lambda}{\xi}$.



Type I & II Revisited:

The Time Dependent G-L Model (TDGL)

- The solution (ψ, \mathbf{A}) minimizes the free energy.
- CGS units (no ϵ_0 or μ_0).

$$\Gamma(\frac{\partial\psi}{\partial t}) + i\kappa\Phi\psi + (|\psi|^2 - (1 - \frac{T}{T_c}))\psi + (-i\frac{\xi}{x_0}\nabla - \frac{x_0}{\lambda}\mathbf{A})^2\psi = 0 \quad (1)$$

$$\sigma(\frac{1}{\lambda^2}\frac{\partial \mathbf{A}}{\partial t} + \nabla \Phi) + \nabla(\nabla \cdot \mathbf{A}) + \nabla \times \nabla \times \mathbf{A} + \frac{i}{2\kappa}(\psi^* \nabla \psi - \psi \nabla \psi^*) + \frac{1}{\lambda^2}|\psi|^2 \mathbf{A} = \nabla \times \mathbf{H}$$
(2)

- + B.C.s and I.C.s
 - **H** is the applied magnetic field.
 - Note $\mathbf{H} = \mathbf{B} \mathbf{M}$; \mathbf{M} =magnetization.
 - σ is the normal conductivity. T is temperature. Γ is relaxation constant.
 - x_0 is scaling factor; Φ the potential is 0 by gauge choice.

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Super and Normal Current

• Two components of the electrical current.

Normal Current Density

The resistive, normal current.

$$\mathsf{J}_n = \sigma \mathsf{E} = \sigma (rac{1}{\lambda} rac{\partial \mathsf{A}}{\partial t} +
abla \Phi)$$

Super Current Density

The resistance free super current.

This is the current that gives rise to the Meissner effect.

$$\mathbf{J}_{s}=-rac{i}{2\kappa}(\psi
abla\psi^{*}-\psi^{*}
abla\psi)-rac{1}{\lambda^{2}}|\psi|^{2}\mathbf{A}$$

Solving The TDGL system

- Non-linear, time dependent, coupled system of PDEs.
- FEM for space. Quadratic triangular elements.
- Quadrature for integrals.
- Adaptive backward Euler for time.
- Newton for non-linearities.
- Direct or Krylov Solver? (SUPERLU_DIST at first)



TDGL Simulation

• $\psi \rightarrow 0$ where the material is normal (vortices or impurities).

• $\lambda = 60 \text{ nm}, \xi = 5 \text{ nm}, (1 - \frac{T}{T_c}) = 0.7, \frac{T}{T_c} = 0.3, \mathbf{H} = 1.5 = 1.5 H_c,$ and $\kappa = 12$.



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TDGL Simulation

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G-L Variants

Anisotropy

Anisotropy can be modeled by assuming electrons have directional dependent masses \rightarrow Effective mass model.

It also creates quantities for each direction: ξ^x , λ^x , κ^x , $H_{c2}^x + [.]^y$

Normal Inclusion

Impurities (Normal Inclusion model) can be modeled as well by solving a second set of equations. This is done by setting the reduced temperature $(1 - \frac{T}{T_c}) = -1$ and removing the $|\psi|^2 \psi$ term.

Applied Current

Applied currents can modeled by modifying the potential Φ .

 $-\sigma\nabla\Phi=\mathbf{J}$

• Modeling Vortex Pinning= Applied Current + Normal Inclusions.

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Anisotropy

• Anisotropy distorts the shape of vortices.

•
$$\lambda^{x} = 60 \text{ nm}, \ \xi^{x} = 5 \text{ nm}, \ (1 - \frac{T}{T_{c}}) = 0.7, \ \frac{T}{T_{c}} = 0.3,$$

 $\mathbf{H} = 1.5 = 1.5\sqrt{2}\mathbf{H}_{c}^{x} \text{ and } \ m_{y} = \frac{1}{4}m_{x}.$



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Anisotropy

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G-L Variants: Normal Inclusion Model

• Superconducting (Ω_s) , Normal (Ω_n) .



Two-Band Superconductivity

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Two-Band Superconductivity

- Some HTS come with odd properties.
- Magnesium Diboride (MgB₂) ($T_c = 39$ K) is no exception.
- Anisotropic direction *ab*.
- Isotropic direction c.
- Upward curvature in T dependence of *H*_{c2}.



Two-Band Superconductivity

- Addition of second superconducting band explained behavior. Bands are "pathways".
- Two-band TDGL model (2B-TDGL) $\rightarrow \psi_1$ and ψ_2 .
- λ_i , ξ_i , κ_i , $H_{i,c2}$, $T_{i,c}$
- Composite T_c , H_{c2} above each band's value from Coupling.
- Peculiarity: $T > T_{2,c}$, but $T < T_{1,c}$ and Superconductivity persists.
- Other HTS (Iron Pnictides) possess similar behavior.

- We would like to model HTS and all their odd properties.
- This composite model includes:
 - Two-band Behavior
 - Anisotropy
 - Applied Currents
 - Novel Strategy for Normal Inclusion
- How to ensure normal behavior?

- For SC $\left(1 \frac{T}{T_c}\right) > 0$
- One-band normals $(1 \frac{T}{T_c}) \rightarrow -1$
- Two-band for MgB₂ $(1 \frac{30K}{T_{2,c}}) \approx -1.5$
- No coupling in normal regions and $(1 \frac{T}{T_{i,c}}) \rightarrow$.

$$\alpha_i(x,y)|_{\Omega_n} < \min\{(1-\frac{T}{T_{1,c}}), (1-\frac{T}{T_{2,c}})\} < 0$$
$$\alpha(x,y) = -2 \in \Omega_n.$$

ND M2B-TDGL

$$\begin{pmatrix} \frac{\partial \psi_1}{\partial t} - i \frac{Jy}{\sigma} \kappa_1 \psi_1 \end{pmatrix} - \alpha_1(x, y) \psi_1 + b(x, y) |\psi_1|^2 \psi_1 \\ + \left(\hat{\mathbf{D}}_1 \cdot \Lambda_1(x, y) \cdot \hat{\mathbf{D}}_1 \right) \psi_1 + \eta(x, y) \psi_2 = 0$$
 (3)

$$\Gamma\left(\frac{\partial\psi_2}{\partial t} - i\frac{Jy}{\sigma}\kappa_1\psi_2\right) - \alpha_2(x,y)\psi_2 + b(x,y)|\psi_2|^2\psi_2 + \left(\hat{\mathbf{D}}_2 \cdot \Lambda_2(x,y) \cdot \hat{\mathbf{D}}_2\right)\psi_2 + \eta(x,y)\nu^2\psi_1 = 0$$
(4)

$$\nabla \times \mathbf{H} + \mathbf{J} = \sigma \frac{\partial \mathbf{A}}{\partial t} + \nabla \times \nabla \times \mathbf{A}$$
$$+ \Lambda_1(x, y) \cdot \left[\frac{i}{2\kappa_1} \left(\psi_1^* \nabla \psi_1 - \psi_1 \nabla \psi_1^*\right) + \frac{x_0^2}{\lambda_{1,c}^2} \mathbf{A} |\psi_1|^2\right]$$
$$+ \Lambda_2(x, y) \cdot \left[\frac{i}{2\nu\kappa_2} \left(\psi_2^* \nabla \psi_2 - \psi_2 \nabla \psi_2^*\right) + \frac{x_0^2}{\lambda_{2,c}^2} \mathbf{A} |\psi_2|^2\right]$$
(5)

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$$\hat{\mathbf{D}}_{1} = -i\frac{\xi_{1,c}}{x_{0}}\nabla - \frac{x_{0}}{\lambda_{1,c}}\mathbf{A}$$
$$\hat{\mathbf{D}}_{2} = -i\frac{\xi_{2,c}}{x_{0}}\nabla - \nu\frac{x_{0}}{\lambda_{2,c}}\mathbf{A}$$
$$\nu = \frac{\lambda_{2,c}\xi_{2,c}}{\lambda_{1,c}\xi_{1,c}}$$

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Modeling MgB₂.

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- MgB₂ is an ideal candidate for our model.
- MgB₂ is cheap and ductile, being ideal for wires.
- Superconducting wires \rightarrow Transport currents.
- Validating our model and it's simulation?
- Flux flow, vortex pinning, and transport currents.

- The material parameters for MgB₂.
- Notice one band is Type II, the other is Type I.
- Γ_i and ϵ (or η) derived.

$\xi_{1,c}{=}13.0 \text{ nm}$	$\lambda_{1,c}{=}$ 47.8 nm	$\kappa_1 = 3.62$
$\xi_{2,c}{=}51.0$ nm	$\lambda_{2,c}{=}33.6$ nm	$\kappa_2 = 0.66$
$\Gamma_1=0.0288\hbar$	$\Gamma_2 = 0.001875\hbar$	ϵ (0K)= -2.7016×10 ⁻¹⁷ J
<i>T_{c1}</i> =35.6 K	<i>T_{c2}</i> =11.8 K	<i>Т_с</i> =39.0 К
$H_{1,c}(0K) = 0.3745 T$	<i>H</i> _{2,<i>c</i>} (0K)=0.1358 T	$ ho_{n}{=}0.7~\mu\Omega/{ m cm}$
$\gamma_1(0K)=4.55$	$\gamma_2(0K)=1.0$	

Validation: Curvature in H_{c2}

- One of the well known properties is the curvature in *H*_{c2}.
- Can we reproduce this in simulations?
- Our coupling is simplified.
- Qualitative behavior.



Vortex Pinning and Transport Currents

- Now we model vortex pinning.
- Our numerical domain.
 (Current +y, Field +z)
- Normal bands (dashed lines) are metal leads.
- We can see how much current is transported resistance free.



• 1. Flux flow with field.

• 2. Vortex pinning.

• 3. Are the normal inclusions pinning?

Simulation 1: Flux Flow in Field

- Now $H = 0.2648 \text{ T}, J = 33.717 \text{ MA cm}^{-2}, T = 30 \text{ K}$
- Movie time frame: 1203.84 ps (1.2 ns)



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Simulation 2: Flux Flow and Normal inclusions

- $H = 0.2648 \text{ T} \text{ J} = 4.214 \text{ MA cm}^{-2}$, T = 30 K.
- 4 Normal Inclusion, outlined in black.



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Simulation 2: Resistance Free Current?

• Super and normal current stream density plots.

Hard to determine!



Average Currents

- We can also look at values in the *y*-direction averaged over *x*.
- There is a large minimum in J_n .



Resistance By Voltage

- Can the voltage be used as a proxy to resistance?
- No Resistance = No Voltage in S.C.! $V(y) = V(0) \int_0^y E_{y,avg}(y')y'$



- J_c is hard to find. Envelope of simulations.
- How can you tell if normal inclusions are working?
- If the vortices are pinned, the voltage change should be small (Metric).
- Implies less flux flow and resistance.

Vortex Pinning

- The normal inclusion arrangement (top) for N= 4, 9, 16, 25 normal inclusions.
- Their respective steady state solutions with H=0.2648 T and $\mathcal{T}=30\text{K}.$ (bottom)



Modeling SC

$J = 0.0843 \text{ MA cm}^{-2} \text{ at } t = 0$

• N=0 has the smallest voltage change at first. Notice the trend with N?



$J = 0.0843 \text{ MA cm}^{-2} \text{ at } 100 \text{ TS}.$

• Now N = 4 and N = 16 have the smallest change due to pinning.



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• While the exact pattern is not known, the normal inclusions pin vortices for mild current densities.

• Δ V in nV

Ν	J=33.717 MA cm ⁻²	$J=0.08429 \text{ MA cm}^{-2}$	J= 0.8429 KA cm ⁻²
0	−326.656 nV	−0.793243 nV	$-5.16257{ imes}10^{-3}~{ m nV}$
4	−326.954 nV	-0.714098 nV	$-6.37429{ imes}10^{-3}$ nV
9	-337.007 nV	-0.782900 nV	$-4.33417{ imes}10^{-3}$ nV
16	-335.168 nV	-0.728167 nV	$-6.97961{ imes}10^{-3}~{ m nV}$

Computational Issues

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Computational Issues

- HTS modeling is only part of the endeavor.
- To simulate superconducting technology, large domains are needed.
- Limited computational resources call for superior methods.
- The needed resolution also grows non-linearly with domain size.
- In this second endeavor, we to hope find ways to improve storage and shorten solve times.
- One-band: $\lambda = 50$ nm, $\xi = 5$ nm, $(1 \frac{T}{T_c}) = 1.0$, $\frac{T}{T_c} = 0.0$, $\mathbf{H} = .15\kappa H_c$, and $\kappa = 10$.

Resolution Issues

- A 300 nm by 300 nm domain. The number of vortices changes with resolution.
- 103040 DOFs and 56 vortices (top left), 231360 DOFs and 59 vortices (top right), 410880 DOFs and 60 vortices (bottom left), and 641600 DOFs and 60 vortices (bottom right)



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Non-Linear Growth in Resolution

Domain sizes of (100 nm)², (200 nm)², (300 nm)², (400 nm)²
h = 4.761 nm for (100 nm)², h = 3.278 nm for (200 nm)², h = 2.127 nm for (300 nm)², and h = 1.990 nm for (400 nm)².



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- Banded solver and symmetric Cholesky solver.
- CSR and SuperLU gave storage improvements.
- Parallelization through Trilinos and distributed matrices.
- Geometry is still a problem.
- Trilinos provides vast suite of solvers (and preconditioners).

- Decoupling methods can reduce memory.
- Decoupling large systems \rightarrow Reducing in DOFs.
- Decoupling ψ and **A** equations?
- This give one non-linear system $(\mathcal{R}\{\psi\}, \mathcal{I}\{\psi\})$ and one linear systems $(\mathbf{A}_x, \mathbf{A}_y)$.

- The storage advantage is clear!
- Going to steady state may take longer with decoupling.
- Global transient behavior.
- Is it more appropriate for dynamic studies?

Domain Expansion

- Now we can see what the improvements have done for us.
- The serial Banded solver limited us to 24 vortices.
- Now we have \approx 450 when the geometry routine maxed out the memory.

Implementation	Method Max	Domain (nm ²)	Domain (ξ^2)	DOFs*	Vortices
		50 ²	$(10\xi)^2$	1,680	0
		100 ²	$(20\xi)^2$	6,560	4
		150 ²	$(30\xi)^2$	58,080	12
Serial	Banded	200 ²	$(40\xi)^2$	58,080	24
		300 ²	$(60\xi)^2$	314,720	60
Serial	CSR Full Eq.	400 ²	$(80\xi)^2$	641,600	116
Serial	CSR Decoup. Type 1	500 ²	$(100\xi)^2$	1,640,960	172
Parallel	Serial Geom max	800 ²	$(160\xi)^2$	23,049,600	\approx 450

A Small Hurdle

120 processors for 96 hours (11520 CPU hours)



800 nm

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- Improve some aspects of the M2B-TDGL.
- More realistic modeling: Normal inclusion metals.
- Apply computational methods to two-band model.

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Type II

• Type II SC have 2 critical values for **H**.

• *H*_{c1}: Transition form Meissner to Vortex state.

• *H*_{c2}: Transition form Vortex to Normal state.

• *H_c* is still used for ND in Type II calculations.



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Modeling SC

• Several we tested on 100 time steps, with 25921 degrees of freedom on a 20 nm by 20 nm domain.

•
$$\lambda = 50$$
 nm, $\xi = 5$ nm, $\kappa = 10$, $(1 - \frac{T}{T_c}) = 1.0$, $\mathbf{H} = 0.15\kappa\sqrt{2}H_c \ \hat{z}$

Preconditioner	NL solver Timing (sec)
Aztec-DD-icc(0)	1193.74
Aztec-DD-ilut(0)	1319.49
ifpack DD-ilu(0)	1332.03
ifpack DD-ilu(2)	1411.68
ML:DD-Aztec-icc(0)	3118.95
ML:DDML-Aztec-icc(0)	3325.07
ML:DDML-Ifpack-ILU(2)	4108.58
ML:DDML-Ifpack-ILU(0)	4319.17

- GMRES iterations for each non-linear solve.
- Aztec-DD-icc has the shortest run time but largest iteration count.
- Iteration count before non-linear tolerance tightened.



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- Iteration counts and solve times?
- How do they perform with more DOFs?

Preconditioner	DOFs	wall time	avg iters per GMRES solve
Aztec-DD-icc(0)			
	103040	1193.74	540.9
	1640960	123479.0	859.0
ifpack DD-ilu(0)			
	103040	1411.68	204.6
	1640960	220355.2	103.3
ML:DD-Aztec-icc(0)			
	103040	3118.95	237.14
	1640960	106508.0	261.6
ML:DDML-Aztec-icc(0)			
	103040	3325.07	237.14
	1640960	47905.8	91.457

- Clearly the ML preconditioners perform well for large domains.
- How do they scale for a small set of processors? (103041 DOFS)



- The Domain Decomposition (DD) and Smooth Aggregation (SA) scale well.
- But have the worst timings.


- The *E J* curve helps characterize *J_c* in Materials.
- Finding *J_c* numerically can be a chore!
- However this observable is still important.



Flux Flow!

```
initialization of time;
set initial time step;
Newton iterates, \psi(0) = \psi_{0,0} and A(0) = A_{0,0,2};
set tol=10^{-8}:
for each time step i do
   Non Linear Solve:
   if steady state then
       STOP:
   else
       update solution and continue;
   end
end
```

Algorithm 1: General TDGL Algorithm

```
Let: G(\psi, \mathbf{A}) be the G-L equation
Let: M(\psi, A) be the Maxwell equation
for k = 1, \dots, k_{max} iterate between equations do
     Solve: Jac[G(\psi_{k,i}, \mathbf{A}_{k,i})]\delta \psi_{k+1,i} = -\text{Resid}[G(\psi_{k,i}, \mathbf{A}_{k,i})];
     \psi_{k+1,i} = \psi_{k,i} + \delta \psi_{k+1,i};
     Solve: M(\psi_{k+1,i}, \mathbf{A}_{k,i}) \mathbf{A}_{k+1,i} = \nabla \times \mathbf{H};
     Calculate: R_1 = \text{Resid}[G(\psi_{k,i+1}, \mathbf{A}_{k,i+1})];
     Calculate: R_2 = \text{Resid}[M(\psi_{k+1,i}, \mathbf{A}_{k,i+1})];
     set Max R=max{R_1, R_2};
     if Max R < tol then
          go to next time step;
     else
          continue iterating;
     end
```

end

Algorithm 2: The decoupling of type 1 algorithm for the TDGL system

Decoupling of Type I Vs Full Equations

- Performance test to steady state.
- Full Equations DOFs: 25920, Decoupling of Type 1 DOFs: 13122.
- Since our matrix size has been reduced by 1/2, our storage is cut by 1/4.
- At the cost of more time steps and non-linear iterations.

Method	Storage	Ti	me steps	Horizon	١	Wall Time
Full	1165896	14	5	5002.05	5	526.226 s
Decoup. type 1	296964	32	8	5477.00	1	463.32 s
Method	NL time (se	ec)	NL time	Avg. (sec))	Avg NL steps
Full	522.459		3.60			1.55
Decoup. type 1	1463.32		4.461	A D > 4 A		3.71

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Decoupling of Type I Vs Full Equations

- The adaptive time step does not give a fair comparison.
- For a fixed non-dimensionalized time step of 0.5.
- Full Equations DOFs: 410,880, Decoupling of type 1 DOFs: 206,082.
- The Decoupling Method gives a shorter solve time! (2 small vs 1 big)

Method	Time steps	NL. Time (sec)	NL time Avg. (sec)	Avg NL steps
Full Eq.	1000	63733.7	63.733	1.455
Decoup. type 1	1000	44974.0	44.974	2.128

- The next clear step is to decouple the TDGL system into 4 four systems.
- This would cut the matrix storage by 1/16 when compared to the full equations.
- Possibly more time steps to steady state.
- What if we just want the steady state?

Decoupling of Type 2

- What if we decouple and linearize using previous time steps (ψ_n, \mathbf{A}_n) .
- Now we have 4 decoupled linear equations.
- Best case scenario?

$$\frac{\partial \psi}{\partial t} - \Delta \psi^{n+1} = -(|\psi^n|^2 - (1 - \frac{T}{T_c})\psi^n - \frac{i}{\kappa}\psi^n \nabla \cdot \mathbf{A}^n - \frac{i}{\kappa}\mathbf{A}^n \cdot \nabla \psi^n - \frac{1}{\lambda^2}\psi^n |\mathbf{A}^n|^2 \text{ in } \Omega \times (0, T) , \quad (6)$$

$$\sigma(\frac{1}{\lambda^2}\frac{\partial \mathbf{A}}{\partial t}) + \nabla \times \nabla \times \mathbf{A}^{n+1} - \nabla(\nabla \cdot \mathbf{A}^{n+1}) = \sigma(\frac{1}{\lambda^2}\frac{\partial \mathbf{A}}{\partial t}) - \Delta \mathbf{A}^{n+1}$$
$$= -\frac{i}{2\kappa}(\psi^n \nabla \psi^{*n} - \psi^{*n} \nabla \psi) - \frac{1}{\lambda^2}|\psi^n|^2 \mathbf{A}^n + \nabla \times \mathbf{H} \text{ in } \Omega \times (0, T) . \quad (7)$$

• Time step size restriction for "backward Euler".

- The restriction has some relations to resolution.
- Could another time method help (Exponential Integrators?)

DOFs	Domain Size (nm ²)	Acceptable Time Step size (ND units)
6561	10 ²	0.5
25921	20 ²	0.3
103041	20 ²	0.3
103041	30 ²	0.0.0625
410881	50 ²	<0.0.0625

• H = 0, J = 33.717 MA cm⁻², T = 30 K, ψ_1 (top), ψ_2 (bottom).

• t = 0.6912 ns, t = 0.6933 ns, t = 0.6974 ns, t = 0.6992 ns.



$J = 33.717 \text{ MA} \text{ cm}^{-2}$

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Resistance Free Current?



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Resistance Free Current?

• \mathbf{J}_s and \mathbf{J}_n in y-direction averaged over x.

• 1/2 of the current is Normal! (J = 33.717 MA cm⁻²)



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